

ELECTROMAGNETIC WAVE PROPAGATION

Wave - In general wave means transporting energy or information.
A wave is a function of both space and time.

Uniform plane wave: A uniform plane wave is defined a wave whose value remains constant throughout a plane which is transverse to the dirⁿ of propagation of the wave.

Properties:

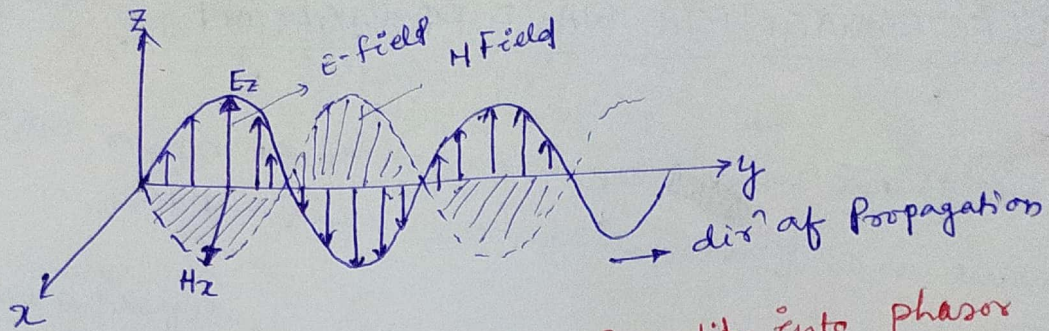
① At every point in space, both E and H are perpendicular to each other and to the dirⁿ of propagation.

A uniform plane wave is the one in which E and H lie in the same plane at any given instant. E and H are uniform over plane surface.

② Velocity of propagation of the wave in free space is $c = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = 3 \times 10^8 \text{ m/s}$.

③ A plane wave is transverse i.e. E and H are transverse (90°) to each other and to the dirⁿ of propagation. Such wave is also called as transverse electromagnetic (TEM).

Ex: If the wave is travelling in z dirⁿ, then the plane $y = \text{const}$ will be perpendicular to the dirⁿ of propagation. In the plane $y = \text{const}$, the variables are x and z . Hence E and H are independent of x and z .



Transformation of a time Varying Quantity into phasor.

Let E_x be the time varying quantities which is either a function of sine or cosine. Then the phasor of E_x is written as E_{xs} and it can be obtained by dropping Re and suppressing $e^{j\omega t}$.

$$\begin{aligned} \text{If } E_x &= E_0 \cos(\omega t + \psi) \\ &= E_0 \text{Real}[\cos(\omega t + \psi) + j \sin(\omega t + \psi)] \\ &= E_0 \text{Real}[e^{j(\omega t + \psi)}] \\ &= E_0 \text{Real}[e^{j\omega t} \cdot e^{j\psi}] \end{aligned}$$

$$\text{Then } E_{xs} = E_0 e^{j\psi}$$

Real means the real part of the following quantity taken.

Further it can be proved that the phasor of $\frac{dE_x}{dt}$ is given by multiplying the phasor of E_x by $j\omega$.

$$\text{Phasor of } \frac{dE_x}{dt} = j\omega E_{xs}$$

Transformation of phasor into a time Varying Quantity.

To transform a phasor into a time varying quantity, multiplying that phasor by $e^{j\omega t}$ and then consider the real part of the product.

$$\begin{aligned} \text{If } E_{xs} &= E_0 e^{j\psi} \text{ then} \\ E_x &= \text{Real}[E_{xs} e^{j\omega t}] \\ &= \text{Real}[E_0 e^{j\psi} e^{j\omega t}] \\ &= \text{Real}[E_0 e^{j(\omega t + \psi)}] \end{aligned}$$

Similarly it can be proved that, the magnetic field intensity is

$$\boxed{\nabla^2 \mathbf{H}_s - \gamma^2 \mathbf{H}_s = 0} \quad \text{--- (2)}$$

The eqn (1) and (2) are known as homogeneous vector Helmholtz's Eqn or simply Vector wave equation.

Since γ in eqn (1) to (2) is a complex quantity.

$$\gamma = \alpha + j\beta \quad \gamma^2 = \alpha^2 + \beta^2$$

$$\gamma = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$$

When we solve it, we get

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} - 1 \right]}$$

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} + 1 \right]}$$

Solution of wave Equations:

The wave eqn for electric field intensity is

$$\nabla^2 \mathbf{E}_s = \gamma^2 \mathbf{E}_s$$

It is vector differential eqn. Let us consider x component of electric field intensity. Then

$$\nabla^2 E_{xs} = \gamma^2 E_{xs}$$

$$\frac{\partial^2 E_{xs}}{\partial x^2} + \frac{\partial^2 E_{xs}}{\partial y^2} + \frac{\partial^2 E_{xs}}{\partial z^2} = \gamma^2 E_{xs}$$

$$\begin{aligned} \nabla \times \mathbf{H}_s &= (\sigma + j\omega\epsilon) \mathbf{E}_s \\ \nabla \times \nabla \times \mathbf{H}_s &= (\sigma + j\omega\epsilon) \nabla \times \mathbf{E}_s \\ \nabla(\nabla \cdot \mathbf{H}_s) - \nabla^2 \mathbf{H}_s &= (\sigma + j\omega\epsilon) \nabla \times \mathbf{E}_s \\ \nabla \times \mathbf{H}_s &= (\sigma + j\omega\epsilon) \nabla \times \mathbf{E}_s \\ \nabla^2 \mathbf{H}_s &= \gamma^2 \mathbf{H}_s \end{aligned}$$

$$\begin{aligned} \nabla \cdot \mathbf{H}_s &= 0 \\ \nabla \cdot \mathbf{B}_s &= 0 \\ \nabla \cdot \mathbf{H}_s &= 0 \end{aligned}$$

$$\boxed{\nabla^2 E_s - \gamma^2 E_s = 0} \quad \text{--- (1)}$$

This is the wave equation for electric field intensity.

Similarly it can be proved that, the wave equation for magnetic field intensity is

$$\boxed{\nabla^2 H_s - \gamma^2 H_s = 0} \quad \text{--- (2)}$$

The eqn (1) and (2) are known as homogeneous vector Helmholtz's eqn or simply vector wave equation.

$$\begin{aligned} \nabla \times H_s &= (\sigma + j\omega\epsilon) E_s \\ \nabla \times \nabla \times H_s &= (\sigma + j\omega\epsilon) \nabla \times E_s \\ \nabla(\nabla \cdot H_s) - \nabla^2 H_s &= (\sigma + j\omega\epsilon) \nabla \times E_s \\ \nabla \times -\nabla^2 H_s &= (\sigma + j\omega\epsilon) \nabla \times E_s \end{aligned}$$

$$\nabla^2 H_s = \gamma^2 H_s$$

$$\begin{aligned} \nabla \cdot H_s &= 0 \\ \therefore \nabla \cdot \frac{B_s}{\mu} &= 0 \\ \therefore \frac{1}{\mu} (\nabla \cdot B_s) &= 0 \end{aligned}$$

Since γ in eqn (1) to (2) is a complex quantity.

$$\gamma = \alpha + j\beta \quad \gamma^2 = \alpha^2 + \beta^2$$

$$\gamma = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$$

When we solve it, we get

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} - 1 \right]}$$

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left[\sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} + 1 \right]}$$

Derivation of wave Equations:

Wave eqn for electric field intensity is

Electric scalar lossy dielectric

Assuming that E_{xs} does not vary with both x and y but varies only with z -variable. We can reduce the equation as

$$\frac{\partial^2 E_{xs}}{\partial z^2} = \gamma^2 E_{xs}$$

* wave is travelling in az dir. E_{xs} will not change with x and y co-ordinates

The solⁿ of the above differential equⁿ may be written as

$$E_{xs} = A e^{-\gamma z}$$

$$[E_{xs} = A e^{-\gamma z} + B e^{\gamma z}]$$

$\downarrow$ along az dir $\downarrow$ along $-az$ dir

Multiplying both sides by $e^{j\omega t}$ and consider the real part. Then we get

But we can consider az dir only. So $B=0$.

$$\begin{aligned} E_x &= \text{Real} [A e^{-\gamma z} e^{j\omega t}] \\ &= \text{Real} [A e^{-(\alpha + j\beta)z} e^{j\omega t}] \\ &= \text{Real} [A e^{-\alpha z} e^{j(\omega t - \beta z)}] \\ &= A e^{-\alpha z} \cos(\omega t - \beta z) \end{aligned}$$

Let E_{x0} be the value of E_x at $t=0$ and $z=0$. Then

$$E_{x0} = A$$

$$E_x = E_{x0} e^{-\alpha z} \cos(\omega t - \beta z)$$

$$E(x, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z)$$

So

$$H(x, t) = H_0 e^{-\alpha z} \cos(\omega t - \beta z)$$

Frequency, wavelength and Intrinsic impedance.

The number of oscillations carried out by a wave at the wave.

Maxwell's Equation in phasor form:

The four Maxwell's equation in point form or differential form are

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} = -\mu \frac{\partial \mathbf{H}}{\partial t}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} = \sigma \mathbf{E} + \epsilon \frac{\partial \mathbf{E}}{\partial t}$$

$$\nabla \cdot \mathbf{D} = \rho_v$$

$$\nabla \cdot \mathbf{B} = 0$$

These eqns in phasor form maybe written as

$$\nabla \times \vec{\mathbf{E}}_s = -j\omega\mu\vec{\mathbf{H}}_s$$

$$\nabla \times \vec{\mathbf{H}}_s = (\sigma + j\omega\epsilon)\vec{\mathbf{E}}_s$$

$$\nabla \cdot \mathbf{D}_s = \rho_v$$

$$\nabla \cdot \mathbf{B}_s = 0$$

Wave Equation for Electric field intensity.

using the vector identity.

$$\nabla \times \nabla \times \mathbf{A} = \nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}$$

$$\nabla \times \nabla \times \mathbf{E}_s = \nabla(\nabla \cdot \mathbf{E}_s) - \nabla^2 \mathbf{E}_s. \quad \text{--- (1)}$$

$$\begin{aligned} \text{LHS} \quad \nabla \times \nabla \times \mathbf{E}_s &= \nabla \times (-j\omega\mu\vec{\mathbf{H}}_s) = -j\omega\mu \nabla \times \vec{\mathbf{H}}_s \\ &= -j\omega\mu(\sigma + j\omega\epsilon)\mathbf{E}_s. \end{aligned}$$

$$\begin{aligned} \text{RHS.} \quad &\nabla(\nabla \cdot \mathbf{E}_s) - \nabla^2 \mathbf{E}_s \\ &= \nabla\left(\nabla \cdot \frac{\mathbf{D}_s}{\epsilon}\right) - \nabla^2 \mathbf{E}_s \\ &= \frac{1}{\epsilon} \nabla(\rho_v) - \nabla^2 \mathbf{E}_s \\ &= -\nabla^2 \mathbf{E}_s. \end{aligned}$$

$$\text{From eqn (1), } \nabla^2 \mathbf{E}_s = j\omega\mu(\sigma + j\omega\epsilon)\mathbf{E}_s.$$

$$\nabla^2 \mathbf{E}_s = \gamma^2 \mathbf{E}_s \text{ where } \gamma^2 = j\omega\mu(\sigma + j\omega\epsilon)$$

the Motion in lossy Dielectric:

A lossy dielectric is a medium in which an EM wave loses power as it propagates due to poor conduction.

A lossy dielectric is characterized by σ (very small), $\mu = \mu_0 \mu_r$, $\epsilon = \epsilon_0 \epsilon_r$.

The Maxwell's equation for time varying fields in phasor is

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} = \mathbf{J}_c + \mathbf{J}_d = \sigma \mathbf{E} + \epsilon \frac{\partial \mathbf{E}}{\partial t}$$

When displacement current ($\mathbf{J}_d = \omega \epsilon \mathbf{E}$) is very much greater than the conduction current, the medium behaves like a dielectric. If $\sigma = 0$, the medium is a perfect lossless dielectric. If $\sigma \neq 0$, the medium is a lossy or imperfect dielectric.

When displacement current density is much greater than conduction current density then the medium is good conductor.

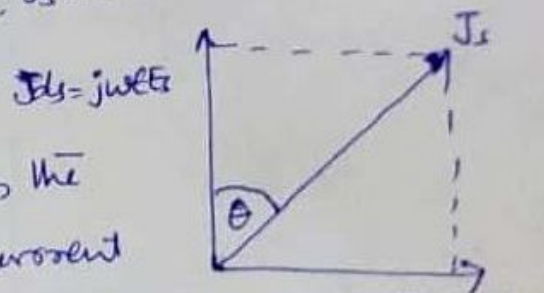
we have

$$\mathbf{J}_c = \nabla \times \mathbf{H}_c = \mathbf{J}_{cs} + \mathbf{J}_{cd}$$

$$= \sigma \mathbf{E}_s + j\omega \epsilon \mathbf{E}_s$$

- * If σ is not zero
- ① $\frac{\sigma}{\omega \epsilon} \ll 1$, good dielectric
 - ② $\frac{\sigma}{\omega \epsilon} \gg 1$, good conductor
 - ③ $\frac{\sigma}{\omega \epsilon} = 1$ quasi conductor

The time phase relationship $\mathbf{J}_{cd}$, $\mathbf{J}_{cs}$, $\mathbf{J}_s$ and $\mathbf{E}_s$ as shown



The angle θ may be identified as the angle by which the displacement current density leads the total current density, we have,

$$\frac{|\mathbf{J}_{cd}|}{|\mathbf{J}_{cs}|} = \frac{|\sigma \mathbf{E}_s|}{|j\omega \epsilon \mathbf{E}_s|} = \frac{\sigma}{\omega \epsilon} = \tan \theta$$

$$\boxed{\tan \theta = \frac{\sigma}{\omega \epsilon}}$$

where $\tan \theta$ is known as loss tangent.

The common power factor angle is the angle by which $\mathbf{J}_c$ leads $\mathbf{E}_s$ is equal to $90^\circ - \theta$.

Wave Motion in Good Conductors

A good conductor is characterized by $\sigma(\text{high}) \gg \omega$.

$$\mu = \mu_0 \text{ (non magnetic conductor)}$$

$$\epsilon = \epsilon_0$$

Since the propagation constant γ is given by

$$\gamma = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$$

$$= \sqrt{j\omega\mu \times j\omega\epsilon \left(1 + \frac{\sigma}{j\omega\epsilon}\right)} = j\omega\sqrt{\mu\epsilon} \sqrt{1 - j\frac{\sigma}{\omega\epsilon}}$$

As $\frac{\sigma}{\omega\epsilon} \gg 1$, $\gamma = j\omega\sqrt{\mu\epsilon} \sqrt{-j\frac{\sigma}{\omega\epsilon}}$

$$\gamma = j\omega \sqrt{\frac{-j\sigma\mu\epsilon}{\omega\epsilon}} = j\omega \sqrt{\frac{-j\sigma\mu}{\omega}}$$

$$\gamma = j \sqrt{-j\sigma\mu\omega} \quad \sqrt{-j} = \sqrt{1 \angle -90^\circ} = 1 \angle -45^\circ = \frac{1}{\sqrt{2}} - j\frac{1}{\sqrt{2}}$$

$$\gamma = j \left(\frac{1}{\sqrt{2}} - j\frac{1}{\sqrt{2}} \right) \sqrt{\omega\mu\sigma} \quad \omega = 2\pi f$$

$$\gamma = \left(\frac{j}{\sqrt{2}} + \frac{1}{\sqrt{2}} \right) \sqrt{2\pi f\mu\sigma}$$

$$\gamma = (1+j) \sqrt{\pi f\mu\sigma}$$

$$\gamma = \sqrt{\pi f\mu\sigma} + j\sqrt{\pi f\mu\sigma} = \alpha + j\beta$$

$$\boxed{\alpha = \beta = \sqrt{\pi f\mu\sigma}}$$

$$\lambda = \frac{\omega}{\beta} = \frac{2\pi f}{\beta} = \frac{2\pi f}{\sqrt{\pi f\mu\sigma}}$$

$$= \frac{2\sqrt{\pi f}}{\sqrt{\mu\sigma}} = \frac{\sqrt{2\omega}}{\sqrt{\mu\sigma}}$$

$$\boxed{\lambda = \frac{\sqrt{2\omega}}{\sqrt{\mu\sigma}}}$$

$$\lambda = \frac{2\pi}{\beta}$$

$$\boxed{\lambda = \frac{2\pi}{\sqrt{\pi f\mu\sigma}}}$$

$$\boxed{\eta = \sqrt{\frac{\mu\omega}{\epsilon} \angle -45^\circ}}$$

$$\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}} = \sqrt{\frac{j\omega\mu}{j\omega\epsilon \left[1 + \frac{\sigma}{j\omega\epsilon}\right]}}$$

$$= \sqrt{\frac{\mu}{\epsilon \left[1 - j\frac{\sigma}{\omega\epsilon}\right]}}$$

$$= \sqrt{\frac{\mu}{\epsilon \times -j\frac{\sigma}{\omega\epsilon}}} = \sqrt{\frac{\mu\omega}{\sigma} \angle -45^\circ}$$

$$\boxed{\eta = \sqrt{\frac{\mu\omega}{\sigma} \angle -45^\circ}}$$

$$\eta = \sqrt{\frac{\mu\omega}{\sigma} \angle -45^\circ}$$

Wave Motion in Free Space;

The free space is characterized by

$$\sigma = 0, \mu = \mu_0, \epsilon = \epsilon_0$$

$$\alpha = 0, \beta = \omega \sqrt{\mu_0 \epsilon_0}$$

$$\eta = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377 = 120 \pi \quad \lambda = \frac{2\pi}{\beta}$$

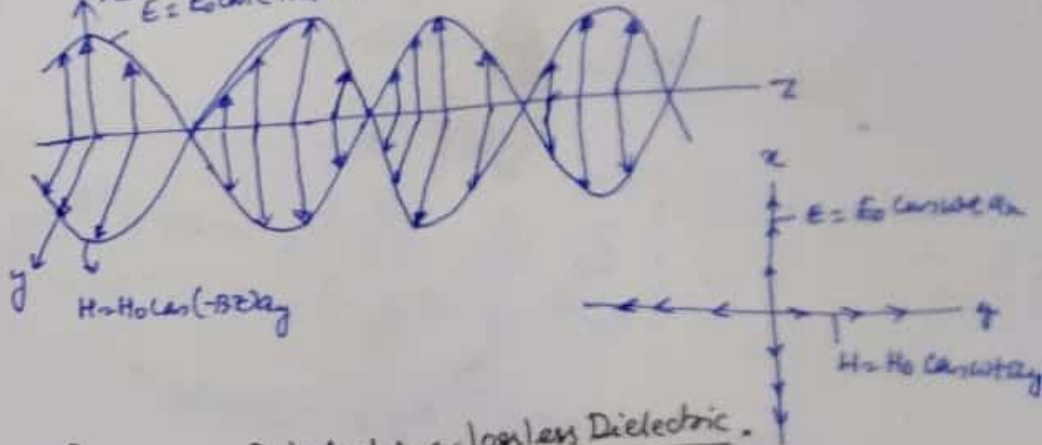
$$v = \frac{\omega}{\beta} = \frac{\omega}{\omega \sqrt{\mu_0 \epsilon_0}} = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = 3 \times 10^8 \text{ m/s}$$

Hence electromagnetic wave in free space travels at speed of light ($3 \times 10^8 \text{ m/s}$).

$$E = E_0 \cos(\omega t - \beta z) \hat{x}$$

$$\text{then } H = H_0 \cos(\omega t - \beta z) \hat{y} = \frac{E_0}{\eta_0} \cos(\omega t - \beta z) \hat{y}$$

$$E = E_0 \cos(\omega t - \beta z) \hat{x}$$
$$H = H_0 \cos(\omega t - \beta z) \hat{y}$$



Wave Motion in Perfect Dielectric / lossless Dielectric.

A Perfect dielectric is characterized by

$$\sigma = 0, \mu = \mu_0 \mu_r, \epsilon = \epsilon_0 \epsilon_r$$

$$\alpha = 0, \beta = \omega \sqrt{\mu_0 \mu_r \epsilon_0 \epsilon_r}$$

$$\eta = \sqrt{\frac{\mu}{\epsilon}} = \sqrt{\frac{\mu_0 \mu_r}{\epsilon_0 \epsilon_r}}$$

$$v = \frac{1}{\sqrt{\mu_0 \mu_r \epsilon_0 \epsilon_r}}$$

Intrinsic Impedance

The ratio of amplitude of electric field intensity to the magnetic field intensity has the dimensions of impedance. This ratio is known as intrinsic impedance of the medium in which the wave is travelling. It is denoted by (η) .

$$\eta = \frac{E}{H}$$

Since the wave equation for electric field intensity is

$$\nabla^2 \vec{E}_s = \gamma^2 \vec{E}_s$$

The solⁿ which is assumed for electric field intensity is

$$E_{xs} = A e^{-\gamma z}$$

$$\vec{E}_s = A e^{-\gamma z} a_x$$

$$\nabla \times \vec{E}_s = -j\omega\mu H_s$$

$$\text{So } \nabla \times \vec{E}_s = \begin{vmatrix} a_x & a_y & a_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A e^{-\gamma z} & 0 & 0 \end{vmatrix} = -A \gamma e^{-\gamma z} a_y$$

$$\text{Hence } -A \gamma e^{-\gamma z} a_y = -j\omega\mu H_s$$

$$H_s = \frac{A \gamma e^{-\gamma z}}{j\omega\mu} a_y$$

$$\eta = \frac{A e^{-\gamma z}}{A \gamma e^{-\gamma z} / j\omega\mu} = \frac{j\omega\mu}{\gamma} = \frac{j\omega\mu}{\sqrt{j\omega\mu(\sigma + j\omega\epsilon)}}$$

$$= \sqrt{\frac{j^2 \omega^2 \mu^2}{j\omega\mu(\sigma + j\omega\epsilon)}} = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$$

$$\boxed{\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}}$$

Wave length :

Wave length means the distance travelled by the wave in which its phase angle changes by 2π radians. It is denoted by λ and units meter.

~~As per Def~~ As per Def $B\lambda = 2\pi$
 $\lambda = \frac{2\pi}{B}$

$B = \text{Phase Const rad/m}$

Velocity -

As $V = f\lambda$ where V is the phase velocity of the wave.

$$V = \frac{\omega}{2\pi} \times \frac{2\pi}{B} = \frac{\omega}{B}$$

$$V = \frac{\omega}{B} \text{ m/sec}$$

Skin effect: (Depth of Penetration)

In a medium of high conductivity, the wave is attenuated as it progresses due to losses which occur in the medium. In a good conductor the rate of attenuation is very great and the wave may penetrate only a very small distance.

The depth of penetration is defined as the depth in which the wave has been attenuated to $\frac{1}{e} = 37\%$ of its initial values.

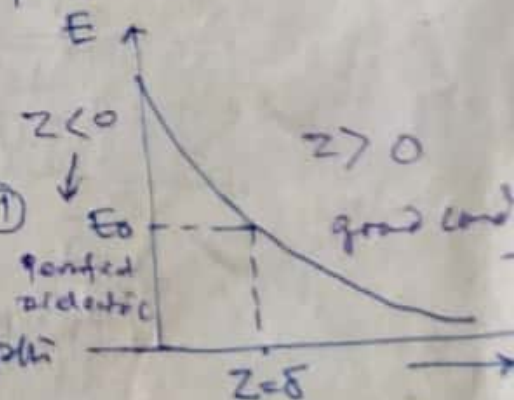
The amplitude of the wave decreases by a factor $e^{-\alpha z}$ where α is attenuation constant.

It is apparent that a distance z which makes $\alpha z = 1$, the amplitude is only $\frac{1}{e}$ times its value at $z=0$.

This distance is equal to δ , the depth of penetration.

we have $\alpha \delta = 1$ ~~$\alpha \delta = 1$~~

$$\delta = \frac{1}{\alpha}$$



The skin δ represents as skin depth which is inversely proportional to attenuation constant.

for a good conductors, $\alpha = \sqrt{\frac{\omega \mu \sigma}{2}}$

$$\text{Skin depth } (\delta) = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega \mu \sigma}} = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

The normal component boundary

Boundary Conditions to Determine the Refraction at the Electric field across the interface



Fig 1

We can use the boundary conditions to determine "Refraction" at the electric field across the interface as shown in Fig 2

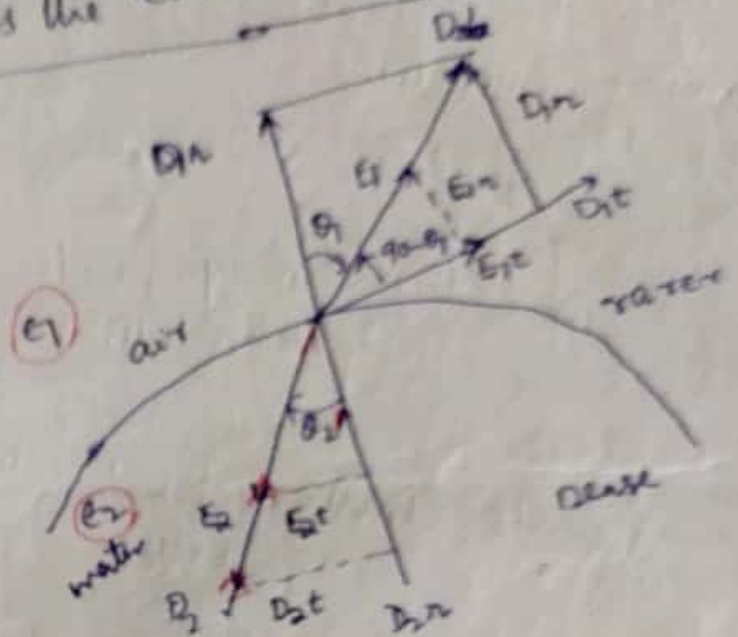


Fig 2

(1) Dielectric-Dielectric

Let D_1 & E_1 makes an angle θ_1 with a normal $D_{n1} \propto E_{n1}$
 Let D_2 & E_2 makes an angle θ_2 with the normal $D_{n2} \propto E_{n2}$
 to the interface as shown in Fig 3

Using normal component of D is continuous across the surface

$$D_{n1} = D_1 \cos \theta_1, \quad D_{n2} = D_2 \cos \theta_2$$

$$D_{n1} = D_{n2}$$

$$D_1 \cos \theta_1 = D_2 \cos \theta_2$$

From

$$\epsilon_1 E_1 \cos \theta_1 = \epsilon_2 E_2 \cos \theta_2$$

(Space for Writing)

The tangential component of $\vec{E}$ are the same on the two sides of the boundary.

$$E_{t1} = E_{t2}$$

$$E_{t1} = E_1 \cos(90^\circ - \theta_1) = E_1 \sin \theta_1$$

$$E_{t2} = E_2 \sin \theta_2$$

$$E_1 \sin \theta_1 = E_2 \sin \theta_2 \quad \text{--- (2)}$$

~~$$E_1 \cos \theta_1 = E_2 \cos \theta_2$$~~

~~from Eqn (1)~~

~~$$\frac{E_1}{E_2} = \frac{\cos \theta_2}{\cos \theta_1}$$~~

from Eqn (2)

~~$$E_2 \sin \theta_2 = E_1 \sin \theta_1$$~~

~~$$D_2 \cos \theta_2 = D_1 \cos \theta_1$$~~

~~$$\frac{D_1 \sin \theta_1}{E_1} = \frac{D_2 \sin \theta_2}{E_2}$$~~

~~$$D_2 \sin \theta_2 = E_2 \sin \theta_2$$~~

~~$$\theta_1^2 + \theta_2^2 = \dots$$~~

~~$$D_2^2 \sin^2 \theta_2 + D_2^2 \cos^2 \theta_2 = \dots$$~~

~~$$D_2 = D_1 \sqrt{\cos^2 \theta_1 + \frac{E_1^2}{E_2^2}}$$~~

Dividing Eqn (2/1)

$$\frac{E_1 \sin \theta_1}{E_1 \cos \theta_1} = \frac{E_2 \sin \theta_2}{E_2 \cos \theta_2}$$

$$\frac{\tan \theta_1}{1} = \frac{\tan \theta_2}{1}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{E_1}{E_2}$$

Since $\epsilon_1 = \epsilon_0 \epsilon_{r1}$
 $\epsilon_2 = \epsilon_0 \epsilon_{r2}$

From Eqn (3)
 $D_1 \cos \theta_1 = D_2 \cos \theta_2$
 From Eqn (4)
 $D_1 \sin \theta_1 = \frac{D_2 E_1 \sin \theta_1}{E_2}$
 $D_1^2 = D_2^2 \left[\cos^2 \theta_2 + \left(\frac{E_1}{E_2} \right)^2 \sin^2 \theta_2 \right]$
 $D_1 = D_2 \sqrt{\cos^2 \theta_2 + \left(\frac{E_1}{E_2} \right)^2 \sin^2 \theta_2}$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1 \epsilon_r}{\epsilon_0 \epsilon_{r2}} \Rightarrow \boxed{\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_{r1}}{\epsilon_{r2}}}$$

This is the law of refraction of the electric field at a boundary free of charge. (since $\rho_s = 0$ is assumed at the interface)

REDMI NOTES 8 - Dielectric Boundary Conditions



- ① A uniform plane wave in a medium having $\sigma = 10^{-3} \text{ S/m}$, $\epsilon = 80\epsilon_0$ and $\mu = \mu_0$ is having a frequency of 10 kHz. Calculate the different parameters of wave.

Sol: $\sigma = 10^{-3} \text{ S/m}$, $\epsilon = 80\epsilon_0$, $\mu = \mu_0$

$$\frac{\sigma}{\omega\epsilon} = \frac{10^{-3}}{2\pi \times 10^4 \times 80 \times 8.85 \times 10^{-12}} = 22.47771.$$

The medium is a good conductor. so attenuation constant

$$\alpha = \sqrt{\pi f \mu \sigma} = \sqrt{\pi \times 10^4 \times 4\pi \times 10^{-7} \times 10^{-3}} = 2\pi \times 10^{-3} \text{ rad/m}$$

Phase constant $\beta = \alpha = 2\pi \times 10^{-3} \text{ rad/m}$.

$$\eta = \sqrt{\frac{\omega\mu}{\sigma}} \angle 45^\circ = 2\pi(1+i) \Omega$$

$$\lambda = \frac{2\pi}{\beta} = 1000 \text{ m}.$$

$$v = \frac{\omega}{\beta} = \frac{2\pi \times 10^4}{2\pi \times 10^{-3}} = 10^7 \text{ m/sec}.$$

- ② The magnetic field intensity of a uniform plane wave in air is 30 A/m in the ay dirⁿ. The wave is propagating in the az dirⁿ at a frequency of $3 \times 10^9 \text{ rad/sec}$. Find
 (a) the wavelength (b) the frequency (c) the period (d) the amplitude

at E. $\beta = \omega \sqrt{\mu_0 \epsilon_0} = 3 \times 10^9 \sqrt{4\pi \times 10^{-7} \times 8.85 \times 10^{-12}} = 10 \text{ rad/m}.$

$$\lambda = \frac{2\pi}{\beta} = \frac{2\pi}{10} = 0.628 \text{ m}$$

$$f = \frac{\omega}{2\pi} = \frac{3 \times 10^9}{2\pi} = 477.464 \text{ MHz}$$

$$T = \frac{1}{f} = 2.094 \text{ nsec}$$

$$\eta = \frac{E}{H} = \sqrt{\frac{\mu_0}{\epsilon_0}} = 376.734$$

$$E = 376.73 \times 30$$

$$E = 11302.03 \text{ V/m}$$

- ③ Determine the Propagation Constant at 400 kHz for a medium $\mu_r = 2$, $\epsilon_r = 17$, and $\sigma = 0$. At what velocity will an electromagnetic wave travel in this medium?

Sol: $f = 400 \text{ kHz}$, $\mu_0 = 2$, $\epsilon_0 = 17$, $\sigma = 0$
 The medium is ~~good~~ ^{perfect} dielectric material, since $\sigma = 0$, ϵ_r is constant

$$\gamma = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)} = j\omega\sqrt{\mu\epsilon}$$

$$\alpha = 0, \quad \beta = \omega\sqrt{\mu\epsilon} = 2\pi f\sqrt{\mu_0\mu_r\epsilon_0\epsilon_r} = 2\pi \times 400 \times 10^3 \sqrt{4\pi \times 10^{-7} \times 2 \times 8.85 \times 10^{-12} \times 17} = 0.0484$$

$$\gamma = \alpha + j\beta, \quad \gamma = 0.0484 \angle 90^\circ$$

$$\text{Velocity of propagation } v = \frac{1}{\sqrt{\mu\epsilon}} = \frac{1}{\sqrt{\mu_0\mu_r\epsilon_0\epsilon_r}} = \frac{1}{\sqrt{\mu_0\epsilon_0} \sqrt{\mu_r\epsilon_r}} = \frac{3 \times 10^8}{\sqrt{2 \times 17}} = 0.57 \times 10^8 \text{ m/sec}$$

④ Determine skin depth for copper with conductivity of 6.6 mmho/meter at 15 MHz frequency.

$$\sigma = 6.6 \text{ mmho/m} \quad f = 15 \text{ MHz}$$

$\mu = \mu_0 \mu_r \rightarrow \mu_0$ Since $\mu_r = 1$ for copper which is a nonmagnetic medium.

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}} = \frac{1}{\sqrt{\pi \times 15 \times 10^6 \times 4\pi \times 10^{-7} \times 6.6 \times 10^6}} = 5.06 \times 10^{-5} \text{ m}$$

⑤ An E field in free space is given by $E = 900 \cos(10^9 t - \beta z) \text{ V/m}$. find (a) β (b) λ (c) H at $P(0.1, 0.5, 0.4)$ at $t = 10 \text{ nsec}$.

$$\omega = 10^9 \quad \beta = \omega\sqrt{\mu_0\epsilon_0} = 3.334 \text{ rad/m}$$

$$\lambda = \frac{2\pi}{\beta} = 1.883 \quad \eta = \frac{E}{H} = 376.7343$$

$$E = 900, \quad H = \frac{900}{376.73} = 2.388 \text{ A/m}$$

$$H = 2.388 \cos(10^9 t - \beta z) \text{ A/m}$$

Since $\vec{E} \times \vec{H} = \text{power}$ direction of propagation along $\vec{E} \times \vec{H}$ direction. $\vec{E}$ is along z means $\vec{H}$ is along x .

Q Two extensive homogeneous dielectrics meet on plane $z=0$. For $z>0$, $\epsilon_1=4$ and for $z<0$ $\epsilon_2=3$.

A uniform electric field $E_1 = 5ax - 2ay + 3az$ kV/m exists for $z>0$. Find

(a) E_2 for $z<0$

(b) The angles θ_1 and θ_2 make the interface.

(c) The energy densities (in J/m²) in both dielectrics.

Sol: (a) Since az is normal to the boundary plane.

$$E_{1n} = E_1 \cdot a_n = E_1 \cdot az = 3$$

$$\vec{E}_{1n} = 3az$$

$$E_{2n} = E_2 \cdot az$$

$$\vec{E}_{2n} = (E_2 \cdot az) az$$

$$E = E_n + E_t$$

$$E_{1t} = E_1 - E_{1n} = (5ax - 2ay + 3az) - 3az$$

$$E_{1t} = 5ax - 2ay$$

$$E_{1t} = E_{2t}$$

$$\Rightarrow E_{2t} = 5ax - 2ay$$

$$D_{2n} = D_{1n} \quad \epsilon_2 E_{2n} = \epsilon_1 E_{1n}$$

$$E_{2n} = \frac{\epsilon_1}{\epsilon_2} E_{1n} = \frac{4}{3} \times 3az = 4az$$

$$E_2 = E_{2t} + E_{2n} = (5ax - 2ay) + 4az \text{ kV/m.}$$

(b) $\alpha_1 = 90 - \theta_1$, $\alpha_2 = 90 - \theta_2$, $E_{1n} = 3$, $E_{1t} = \sqrt{25+4} = \sqrt{29}$

$$\tan \alpha_1 = \frac{E_{1t}}{E_{1n}} = \frac{\sqrt{29}}{3} = 1.795, \quad \theta_1 = 60.9^\circ$$

$$\alpha_1 = 29.1^\circ$$

$$E_{2n} = 4, \quad E_{2t} = E_{1t} = \sqrt{29}, \quad \tan \alpha_2 = \frac{E_{2t}}{E_{2n}} = \frac{\sqrt{29}}{4} = 1.346$$

$$\alpha_2 = 53.4^\circ, \quad \theta_2 = 36.6^\circ$$

$$\tan \theta_1 = \frac{\epsilon_1}{\epsilon_2} \tan \theta_2 \quad (\text{in surface})$$

(c) $w_{E1} = \frac{1}{2} \epsilon_1 (E_1)^2 = \frac{1}{2} \times 4 \times 10^{-9} \times (25+4+9) \times 10^6$

Polarization:

The polarization of a uniform plane wave refers to the time varying behaviour of the electric field intensity at some fixed point in space.

There are three types of polarization

- ① Linear polarization
- ② Elliptical polarization
- ③ Circular polarization.

Elliptical polarization:

Let E_x = instantaneous electric field of the horizontal polarized wave (component)
 E_y = instantaneous electric field of the vertically polarized wave (component).

Then the electric field component as a function of time and distance in x and y dirⁿ are

$$\left. \begin{aligned} E_x &= E_1 \sin(\omega t - \beta z) \\ E_y &= E_2 \sin(\omega t - \beta z + \delta) \end{aligned} \right\} \text{--- ①}$$

Where E_1, E_2 are amplitudes of plane polarized wave in x and y dirⁿ respectively and δ the time phase angle by which E_y leads E_x .

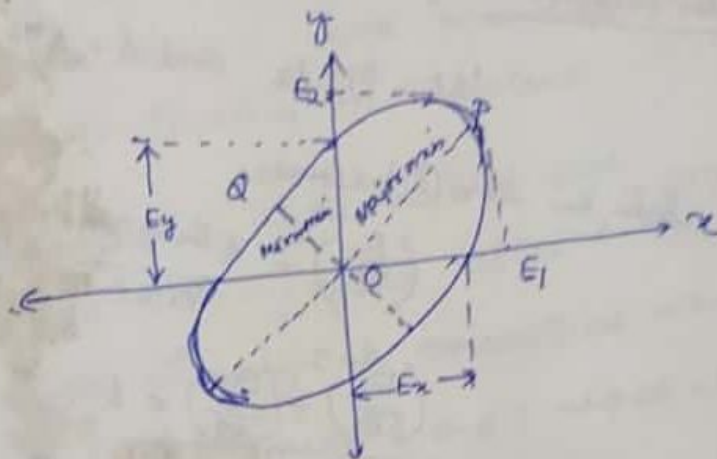
Now $E = E_x \hat{a}_x + E_y \hat{a}_y$

At $z=0$ the eqnⁿ ① becomes

$$\begin{aligned} E_x &= E_1 \sin \omega t \\ E_y &= E_2 \sin(\omega t + \delta) \end{aligned}$$

The Eqnⁿ which represent an the general form of ellipse. (2)

OP = Semi major axis.
 OQ = Semi minor axis.



Linear Polarization:

Let E_y be in phase or 180° out of phase with E_x then $\delta = 0$,

The lawⁿ (2-1) becomes

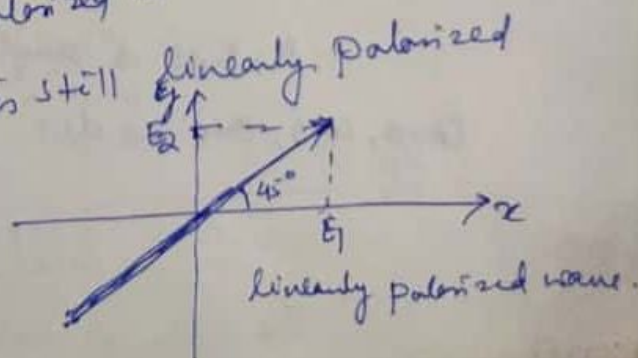
$$\left(\frac{E_y}{a}\right)^2 \pm \frac{2E_y}{E_1 E_2} + \left(\frac{E_x}{E_1}\right)^2 = 0$$

$$\left(\frac{E_y}{E_2} \pm \frac{E_x}{E_1}\right)^2 = 0$$

$$\frac{E_y}{E_2} = \pm \frac{E_x}{E_1} \quad E_y = \pm \frac{E_2}{E_1} E_x$$

$$E_y = \frac{E_2}{E_1} E_x \quad \boxed{E_y = M E_x} \quad \text{--- (4)}$$

This lawⁿ (4) represent a straight line where $m = \frac{E_2}{E_1}$ = slope of the line. Hence when two linearly polarized component waves are in phase or out of phase, the resultant wave is a plane (ordinarily) polarized with E . If $E_1 = 0$, the wave is polarized in y-dirⁿ and when $E_2 = 0$, the wave is polarized in x-dirⁿ and when $E_1 = E_2$, and $\delta = 0$, the wave is still linearly polarized but at 45° .



Circular polarization:

let $E_1 = E_2$ and $\delta = \pm 90^\circ$.

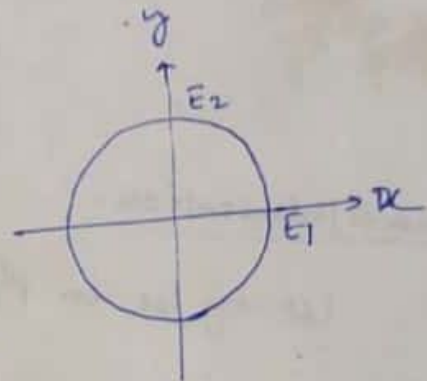
Then the eqn (3) becomes

$$\left(\frac{E_x}{E_1}\right)^2 - \frac{2E_xE_y \cos 90^\circ}{E_1E_2 \sin 90^\circ} + \left(\frac{E_y}{E_1}\right)^2 = 1.$$

$$\left(\frac{E_x}{E_1}\right)^2 + \left(\frac{E_y}{E_1}\right)^2 = 1$$

$$E_x^2 + E_y^2 = E_1^2 \quad \text{--- (4)}$$

$$E_x^2 + E_y^2 = E_2^2$$



The eqn (4) and the eqn (5) are circles.

Therefore, when two linearly polarized component waves are in time phase quadrature (i.e. 90°) and also are equal in magnitude, the resultant wave is circularly polarized.

Direction Cosine:

The uniform plane wave travelling in x-dirⁿ is given by

$$E(x) = E_0 e^{-j\beta x}$$

The plane at constant phase is given by $x = \text{constant}$

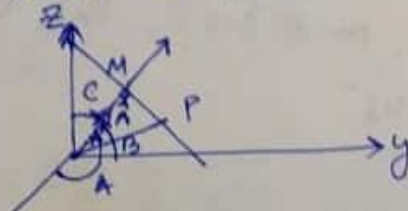
For a plane wave travelling in arbitrary dirⁿ then the equation of the plane is $\hat{n} \cdot \vec{r} = \text{const}$ where $\vec{r}$ is radius vector from the origin to the point P.

$$\hat{n} \cdot \vec{r} = x \cos A + y \cos B + z \cos C$$

$$\text{where } \vec{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z.$$

A, B, C $\rightarrow$ angle that the unit vector makes with x, y and z axes

$\cos A, \cos B, \cos C \rightarrow$ dirⁿ cosines or dirⁿ components of the vector.



Reflection by Perfect Dielectric (Normal incidence)

(3)

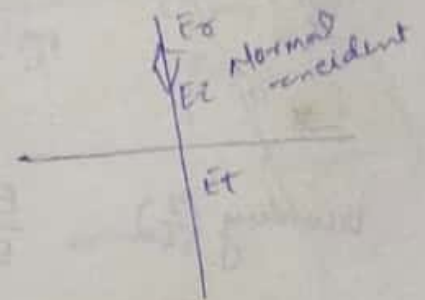
Let us consider the two media with parameters ϵ_1, μ_1 and ϵ_2, μ_2 . The boundary is parallel to $x=0$ plane.

$E_i \rightarrow$ electric field intensity of the incident wave.

$E_r \rightarrow$ electric field intensity of the reflected wave.

$E_t \rightarrow$ electric field intensity of transmitted wave.

η_1, η_2 are the impedances of the media 1 and 2 respectively and it is given by $\eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}}$ and $\eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}}$.



$$E_i = \eta_1 H_i \quad \text{--- (1)}$$

$$E_r = -\eta_1 H_r \quad \text{--- (2)}$$

$$\text{and } E_t = \eta_2 H_t \quad \text{--- (3)}$$

Since the total field in medium (1) comprises both incident and reflected fields, whereas medium 2 has only transmitted field.

$$\text{So } E_i + E_r = E_t$$

$$\text{and } H_i + H_r = H_t$$

$$\text{From eqn (3), } H_t = \frac{E_t}{\eta_2} = \frac{1}{\eta_2} [E_i + E_r]$$

$$H_i + H_r = \frac{1}{\eta_2} [E_i + E_r]$$

$$\Rightarrow \frac{E_i}{\eta_1} - \frac{E_r}{\eta_1} = \frac{1}{\eta_2} [E_i + E_r]$$

$$\left[\frac{1}{\eta_1} - \frac{1}{\eta_2} \right] E_i = \left[\frac{1}{\eta_2} + \frac{1}{\eta_1} \right] E_r$$

$$\frac{\eta_2 - \eta_1}{\eta_1 \eta_2} E_i = \frac{\eta_1 + \eta_2}{\eta_1 \eta_2} E_r$$

$$\boxed{\frac{E_r}{E_i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}} \quad \text{--- (5)}$$

$$T = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \text{ --- reflection coefficient}$$

As we know that $E_i + E_r = E_t$

$$1 + \frac{E_r}{E_i} = \frac{E_t}{E_i}$$

$$\Rightarrow \frac{E_t}{E_i} = 1 + \frac{E_r}{E_i} = 1 + \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

$$\boxed{\frac{E_t}{E_i} = \frac{2\eta_2}{\eta_1 + \eta_2}} \quad \text{--- (6)}$$

$$\tau = \frac{E_t}{E_i} = \frac{2\eta_2}{\eta_1 + \eta_2} = \text{Transmission coefficient.}$$

Dividing (2/1)

$$\frac{E_r}{E_i} = -\frac{H_r}{H_i}$$

$$\frac{H_r}{H_i} = -\frac{E_r}{E_i} = -\left[\frac{\eta_2 - \eta_1}{\eta_1 + \eta_2}\right] = \frac{\eta_1 - \eta_2}{\eta_1 + \eta_2}$$

$$\boxed{\frac{H_r}{H_i} = \frac{\eta_1 - \eta_2}{\eta_1 + \eta_2}}$$

Dividing (3/4),

$$\frac{E_t}{E_i} = \frac{\eta_2 H_t}{\eta_1 H_i}$$

$$\frac{H_t}{H_i} = \frac{\eta_1}{\eta_2} \frac{E_t}{E_i} = \frac{\eta_1}{\eta_2} \times \frac{2\eta_2}{\eta_1 + \eta_2}$$

$$\boxed{\frac{H_t}{H_i} = \frac{2\eta_1}{\eta_1 + \eta_2}}$$

Wave Incident obliquely on boundary betⁿ Perfect Dielectric

Let us consider an incident wave meets on the boundary over the region AB and gets partly reflected and partly transmitted. The incident ray FA, the reflected ray AD and transmitted ray AE all lies in one plane, θ_i , θ_r and θ_t are the angles of incident, reflected and transmitted wave respectively.



REDMI NOTE 8

AI QUAD CAMERA

The normal NAN' to the boundary at the point A, then we can draw AC perpendicular to the incident wave, AD perpendicular to reflected wave and AE perpendicular to transmitted wave.

Let ϵ_1 and ϵ_2 be the permittivities of medium 1 and 2 and μ_0 and μ_2 be the permeabilities of both media. Since the permeability of all known dielectric is same as for free space.

Then the velocities of propagation of wave in the two media will be

$$V_1 = \frac{1}{\sqrt{\mu_0 \epsilon_1}}, \quad V_2 = \frac{1}{\sqrt{\mu_0 \epsilon_2}}$$

Let us assume that the incident beam reaches the point A at time t_1 and the point B at time t_2 , then

$$\left. \begin{aligned} CB &= V_1 (t_2 - t_1) \\ AD &= V_1 (t_2 - t_1) \\ AE &= V_2 (t_2 - t_1) \end{aligned} \right\} \text{--- (1)}$$

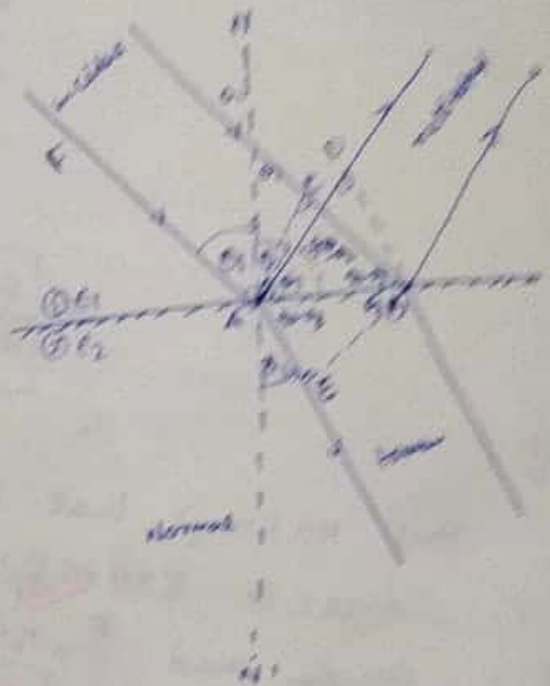
But from the above fig, $\angle NAF = \theta_1 = \angle BAC$
 $\angle NAD = \theta_2 = \angle ADE$
 $\angle N'AE = \theta_3 = \angle ABE$

From (1) $BC = AD$.

$$\Rightarrow AB \sin \theta_1 = AB \sin \theta_2$$

$$\boxed{\theta_1 = \theta_2}$$

This is Snell's law of refraction showing that the angle of incidence is



from eqn ① $\frac{CB}{AE} = \frac{V_1}{V_2}$

$$\frac{AB \sin \theta_1}{AB \sin \theta_3} = \frac{V_1}{V_2}$$

$$\frac{\sin \theta_1}{\sin \theta_3} = \frac{V_1}{V_2}$$

Part $V_1 = \frac{1}{\sqrt{\mu_0 \epsilon_1}}$

$$V_2 = \frac{1}{\sqrt{\mu_0 \epsilon_2}}$$

$$\Rightarrow \boxed{\frac{\sin \theta_1}{\sin \theta_3} = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}}} \xrightarrow{\text{Snell's law}} \frac{V_1}{V_2} = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}} \quad \text{--- ②}$$

But we know that the power flow in the dirⁿ of P which is equal to $E \times H$. Since in the wave E and H are at right angles and $\frac{E}{H} = \eta$, Therefore the power is equal to $EH \sin 90^\circ$
 $= EH = \frac{E^2}{\eta}$

Let us consider the component of power flowing in the dirⁿ at the normal NAN' , we get

$$\frac{E_i^2}{\eta_1} \cos \theta_1 - \frac{E_r^2}{\eta_1} \cos \theta_2 = \frac{E_t^2}{\eta_2} \cos \theta_3$$

Now dividing throughout $\frac{E_i^2}{\eta_1} \cos \theta_1$ and $(\theta_1 = \theta_2)$

$$1 = \frac{E_r^2}{E_i^2} + \frac{\eta_1 \cos \theta_3}{\eta_2 \cos \theta_1} \left(\frac{E_t}{E_i} \right)^2$$

$$1 - \frac{E_r^2}{E_i^2} = \frac{\eta_1 \cos \theta_3}{\eta_2 \cos \theta_1} \left(\frac{E_t}{E_i} \right)^2$$

$$\boxed{\frac{E_r^2}{E_i^2} = 1 - \frac{\eta_1 \cos \theta_3}{\eta_2 \cos \theta_1} \left(\frac{E_t}{E_i} \right)^2} \quad \text{--- ③}$$

perpendicular polarization:

$$\begin{aligned}
 T_{\perp} &= \frac{\sin(\theta_3 - \theta_1)}{\sin(\theta_3 + \theta_1)} \\
 &= \frac{\sin \theta_3 \cos \theta_1 - \cos \theta_3 \sin \theta_1}{\sin \theta_3 \cos \theta_1 + \cos \theta_3 \sin \theta_1} \\
 &= \frac{\cos \theta_1 - \cos \theta_3 \cdot \frac{\sin \theta_1}{\sin \theta_3}}{\cos \theta_1 + \cos \theta_3 \cdot \frac{\sin \theta_1}{\sin \theta_3}} = \frac{\cos \theta_1 - \cos \theta_3 \cdot \frac{n_1}{n_2}}{\cos \theta_1 + \cos \theta_3 \cdot \frac{n_1}{n_2}} \\
 &= \frac{n_2 \cos \theta_1 - n_1 \cos \theta_3}{n_2 \cos \theta_1 + n_1 \cos \theta_3} = \frac{E_r}{E_i}
 \end{aligned}$$

$$\text{But } \frac{\sin \theta_1}{\sin \theta_3} = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}}$$

$$n_1 = \frac{1}{\sqrt{\epsilon_1}}, n_2 = \frac{1}{\sqrt{\epsilon_2}}, \frac{n_1}{n_2} = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}}$$

parallel polarization:

$$T_{\parallel} = \frac{\tan(\theta_3 - \theta_1)}{\tan(\theta_3 + \theta_1)} = \frac{\sin(\theta_3 - \theta_1)}{\cos(\theta_3 - \theta_1)} \times \frac{\cos(\theta_3 + \theta_1)}{\sin(\theta_3 + \theta_1)}$$

$$= \frac{2 \sin(\theta_3 - \theta_1) \cos(\theta_3 + \theta_1)}{2 \cos(\theta_3 - \theta_1) \sin(\theta_3 + \theta_1)}$$

$$= \frac{\sin(2\theta_3) + \sin(-2\theta_1)}{\sin(2\theta_3) - \sin(-2\theta_1)}$$

$$= \frac{2 \sin \theta_3 \cos \theta_3 - 2 \sin \theta_1 \cos \theta_1}{2 \sin \theta_3 \cos \theta_3 + 2 \sin \theta_1 \cos \theta_1}$$

$$= \frac{\cos \theta_3 - \cos \theta_1 \cdot \frac{\sin \theta_1}{\sin \theta_3}}{\cos \theta_3 + \cos \theta_1 \cdot \frac{\sin \theta_1}{\sin \theta_3}}$$

$$= \frac{\cos \theta_3 - \cos \theta_1 \cdot \frac{n_1}{n_2}}{\cos \theta_3 + \cos \theta_1 \cdot \frac{n_1}{n_2}}$$

$$= \frac{n_2 \cos \theta_3 - n_1 \cos \theta_1}{n_2 \cos \theta_3 + n_1 \cos \theta_1} =$$

① Perpendicular polarization.

As we know that $E_i + E_r = E_t$

$$\frac{E_t}{E_i} = 1 + \frac{E_r}{E_i}$$

Now substituting $\frac{E_t}{E_i}$ in Eqn (3).

$$\begin{aligned}\frac{E_r^2}{E_i^2} &= 1 - \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} \left(\frac{E_t}{E_i} \right)^2 \\ &= 1 - \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} \left(1 + \frac{E_r}{E_i} \right)^2\end{aligned}$$

$$\Rightarrow 1 - \frac{E_r^2}{E_i^2} = \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} \left(1 + \frac{E_r}{E_i} \right)^2$$

$$\Rightarrow \left(1 + \frac{E_r}{E_i} \right) \left(1 - \frac{E_r}{E_i} \right) = \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} \left(1 + \frac{E_r}{E_i} \right)^2$$

$$1 - \frac{E_r}{E_i} = \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} \left(1 + \frac{E_r}{E_i} \right)$$

$$1 - \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} = \frac{E_r}{E_i} \left(1 + \frac{n_1 \cos \theta_3}{n_2 \cos \theta_1} \right)$$

$$\frac{n_2 \cos \theta_1 - n_1 \cos \theta_3}{n_2 \cos \theta_1} = \frac{E_r}{E_i} \left(\frac{n_2 \cos \theta_1 + n_1 \cos \theta_3}{n_2 \cos \theta_1} \right)$$

$$\boxed{\frac{E_r}{E_i} = \frac{n_2 \cos \theta_1 - n_1 \cos \theta_3}{n_2 \cos \theta_1 + n_1 \cos \theta_3}}$$

$T_{\perp} = \frac{E_t}{E_i} =$ Reflection co-efficient for perpendicular polarization.

$$\text{Ans} \quad \frac{E_t}{E_i} = 1 + \frac{E_r}{E_i} = 1 + \frac{n_2 \cos \theta_1 - n_1 \cos \theta_3}{n_2 \cos \theta_1 + n_1 \cos \theta_3}$$

Apply the boundary cond that the E must be the same value on both sides of the boundary of medium ① and medium ②, hence $\theta_1 = \theta_2$.

$$E_i \cos \theta_1 - E_r \cos \theta_1 = E_t \cos \theta_2$$

$$\Rightarrow E_i \cos \theta_1 = E_r \cos \theta_2 + E_t \cos \theta_2$$

Dividing throughout by $E_i \cos \theta_1$

$$1 = \frac{E_r}{E_i} + \frac{E_t \cos \theta_2}{E_i \cos \theta_1}$$

$$1 - \frac{E_r}{E_i} = \frac{E_t \cos \theta_2}{E_i \cos \theta_1}$$

$$\Rightarrow \frac{E_t}{E_i} = \left(1 - \frac{E_r}{E_i}\right) \frac{\cos \theta_1}{\cos \theta_2} \quad \text{--- (4)}$$

But from Equ (3), $\frac{E_r}{E_i} = 1 - \frac{\eta_1 \cos \theta_2}{\eta_2 \cos \theta_1} \left(\frac{E_t}{E_i}\right)^2$

$$\Rightarrow \frac{\eta_1 \cos \theta_2}{\eta_2 \cos \theta_1} \left(\frac{E_t}{E_i}\right)^2 = 1 - \frac{E_r}{E_i}$$

$$\Rightarrow \frac{\eta_1 \cos \theta_2}{\eta_2 \cos \theta_1} \left(1 - \frac{E_r}{E_i}\right)^2 \frac{\cos \theta_1}{\cos \theta_2} = \left(1 + \frac{E_r}{E_i}\right) \left(1 - \frac{E_r}{E_i}\right)$$

$$\frac{\eta_1 \cos \theta_1}{\eta_2 \cos \theta_2} \left(1 - \frac{E_r}{E_i}\right) = 1 + \frac{E_r}{E_i}$$

$$\frac{\eta_1 \cos \theta_1}{\eta_2 \cos \theta_2} - 1 = \frac{E_r}{E_i} \left[1 + \frac{\eta_1 \cos \theta_1}{\eta_2 \cos \theta_2}\right]$$

$$\frac{\eta_1 \cos \theta_1 - \eta_2 \cos \theta_2}{\eta_2 \cos \theta_2} = \frac{E_r}{E_i} \left[\frac{\eta_2 \cos \theta_2 + \eta_1 \cos \theta_1}{\eta_2 \cos \theta_2} \right]$$

$$\boxed{\frac{E_r}{E_i} = \frac{\eta_1 \cos \theta_1 - \eta_2 \cos \theta_2}{\eta_1 \cos \theta_1 + \eta_2 \cos \theta_2}} = T_{II} \quad \text{--- (5)}$$

Brewster angle :

This is the angle of incidence for which angle of reflection is zero. i.e. $\frac{E_r}{E_i} = 0$.

From equⁿ (5), $\eta_1 \cos \theta_1 = \eta_2 \cos \theta_3$
 $\eta_1^2 \cos^2 \theta_1 = \eta_2^2 \cos^2 \theta_3 = \eta_2^2 (1 - \sin^2 \theta_3)$

But from Snell's Equⁿ $\frac{\sin \theta_1}{\sin \theta_3} = \frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_1}}$

$$\Rightarrow \sin \theta_3 = \frac{\sqrt{\epsilon_1}}{\sqrt{\epsilon_2}} \sin \theta_1$$

$$\therefore \eta_1^2 \cos^2 \theta_1 = \eta_2^2 \left[1 - \frac{\epsilon_1}{\epsilon_2} \sin^2 \theta_1 \right]$$

$$\eta_1^2 = \eta_2^2 \left[\frac{1}{\cos^2 \theta_1} - \frac{\epsilon_1}{\epsilon_2} \frac{\sin^2 \theta_1}{\cos^2 \theta_1} \right]$$

$$\eta_1^2 = \eta_2^2 \left[\sec^2 \theta_1 - \frac{\epsilon_1}{\epsilon_2} \tan^2 \theta_1 \right]$$

$$\eta_1^2 = \eta_2^2 (1 + \tan^2 \theta_1) - \eta_2^2 \frac{\epsilon_1}{\epsilon_2} \tan^2 \theta_1$$

$$\eta_1^2 = \eta_2^2 + \eta_2^2 \tan^2 \theta_1 - \eta_2^2 \frac{\epsilon_1}{\epsilon_2} \tan^2 \theta_1$$

$$\eta_1^2 - \eta_2^2 = \eta_2^2 \tan^2 \theta_1 \left[1 - \frac{\epsilon_1}{\epsilon_2} \right]$$

$$\frac{\mu_0}{\epsilon_1} - \frac{\mu_0}{\epsilon_2} = \frac{\mu_0}{\epsilon_2} \tan^2 \theta_1 \left[\frac{\epsilon_2 - \epsilon_1}{\epsilon_2} \right]$$

$$\frac{\epsilon_2 - \epsilon_1}{\epsilon_1 \epsilon_2} = \frac{1}{\epsilon_2} \tan^2 \theta_1 \left[\frac{\epsilon_2 - \epsilon_1}{\epsilon_2} \right]$$

$$\tan^2 \theta_1 = \frac{\epsilon_2}{\epsilon_1}$$

$$\tan \theta_1 = \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

$$\theta_1 = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

This is called Brewster angle. For this angle of incidence in this case there is no reflected ray, and the entire